

Remember that a mechanical system without friction or an electrical system without resistance can be expressed in the Hamiltonian form.

$$H = \frac{1}{2} k x^2 + \frac{1}{2} M \dot{x}^2$$

$$H = \frac{1}{2C} q^2 + \frac{1}{2} L \dot{q}^2$$

$$(x, M\dot{x}) \leftarrow (p, q) \rightarrow (q, L\dot{q})$$

$$\begin{aligned} \dot{q} &= \frac{\partial H}{\partial p} \\ \dot{p} &= -\frac{\partial H}{\partial q} + f \end{aligned}$$

$q$ : Generalized Coordinate/Position

$p$ : Generalized Momentum

$f$ : Generalized Force (Effort)

↪ Force/Torque/Voltage etc

→ Then we can define the rate at which electrical/mechanical work is being done.

$$S = \langle f, \dot{q} \rangle = f^T \dot{q}$$

It is also known as the Supply Rate.

Then, time rate of change of the Hamiltonian  $H$  can be expressed as —

$$\begin{aligned} \dot{H} &= \left( \frac{\partial H}{\partial q} \right)^T \dot{q} + \left( \frac{\partial H}{\partial p} \right)^T \dot{p} \\ &= \left( \frac{\partial H}{\partial q} \right)^T \left( \frac{\partial H}{\partial p} \right) + \left( \frac{\partial H}{\partial p} \right)^T \left( -\frac{\partial H}{\partial q} \right) + \left( \frac{\partial H}{\partial p} \right)^T f \\ &= \dot{q}^T f = S \end{aligned}$$

Thus the stored energy of the system ( $H$ ) changes at a rate same as the supply rate  $S$ . One can interpret the supply rate as the power input to the system.

In general if there is any dissipation (i.e. loss of stored energy) due to damping/friction/resistance, we have the following relationship-

$$\boxed{\frac{dH}{dt} \leq S.} \quad \text{---} \quad \textcircled{2}$$

Then, by treating the generalized forces and velocities as inputs and outputs respectively, we have the following (weaker) version of (2), known as the dissipation inequality:

$$\boxed{H(q(t), p(t)) \leq H(q(0), p(0)) + \int_0^t u^T(\tau) y(\tau) d\tau} \quad \textcircled{3}$$

where,  $u \triangleq f$  and  $y \triangleq \dot{q}$ .

Moreover, if the Hamiltonian is bounded below, i.e.  $H(q, p) \geq c$  for every  $q, p$ , (3) can be expressed as —

$$\begin{aligned} \int_0^t u^T(\tau) y(\tau) d\tau &\geq H(q(t), p(t)) - H(q(0), p(0)) \\ &\geq c - H(q(0), p(0)) \\ &= -\delta \end{aligned}$$

where  $\delta \triangleq H(q(0), p(0)) - c \geq 0$  depends on the initial condition.

# PASSIVITY AND DISSIPATIVE SYSTEMS:—

In what follows we will see a further generalization of this concept. Here we consider nonlinear systems with dynamics given by —

$$\begin{aligned} \dot{x} &= f(x, u) \\ y &= h(x, u) \end{aligned} \quad \text{--- (4)}$$

where,  $x(t) \in \mathbb{R}^n$ ,  $u(t) \in U \subset \mathbb{R}^m$  and  $y(t) \in Y \subset \mathbb{R}^p$  at every  $t \geq 0$ , together with a function

$$\begin{aligned} s: U \times Y &\rightarrow \mathbb{R} \\ (u(t), y(t)) &\mapsto s(u(t), y(t)), \end{aligned} \quad \text{--- (5)}$$

which we call the supply rate of (4).

→ System (4) is called to be dissipative with respect to the supply rate  $s$  if there exists a function  $\Phi: \mathbb{R}^n \rightarrow [0, \infty)$ , called the storage function, such that for all  $t_1 \geq t_0$  and any  $x(t_0) \in \mathbb{R}^n$  and any input function  $u(\cdot)$ , we have —

$$\Phi(x(t_1)) \leq \Phi(x(t_0)) + \int_{t_0}^{t_1} s(u(\tau), y(\tau)) d\tau \quad \text{--- (6)}$$

where  $x(t_1)$  is the state of (4) at time  $t_1$  resulting from the initial condition  $x(t_0)$  at time  $t_0$  under the input  $u(\cdot)$ . Condition (6) is the more general form of dissipation inequality.

→ As discussed in the last class, a nonlinear system can also be viewed as a function or a map between two appropriate function spaces; more specifically between extended  $L_\infty$ -spaces.

Consider,  $G: L_{2e} \rightarrow L_{2e}$ . Then,  $G$  is passive if there exists some constant  $\beta \in \mathbb{R}$  such that —

$$\int_0^t u^T(\tau) (G(u))(\tau) d\tau \geq \beta$$

for every  $u \in L_{2e}$  and  $t \geq 0$ . Moreover,  $G$  is strictly input passive if there exists  $\beta \in \mathbb{R}$  and  $\delta > 0$  such that —

$$\int_0^t u^T(\tau) (G(u))(\tau) d\tau \geq \delta \int_0^t u^T(\tau) u(\tau) d\tau + \beta$$

for every  $u \in L_{2e}$  and  $t \geq 0$ .  $G$  is strictly output passive if there exist  $\beta \in \mathbb{R}$  and  $\delta > 0$  such that,

$$\int_0^t u^T(\tau) (G(u))(\tau) d\tau \geq \delta \int_0^t (G(u))^T(\tau) (G(u))(\tau) d\tau + \beta$$

for every  $u \in L_{2e}$  and  $t \geq 0$ .

Then we can say that the system (4) is passive if it is dissipative with respect to the supply rate —

$$s(u(t), y(t)) = u^T(t) y(t).$$

Moreover, (4) is strictly input passive if there exists  $\delta > 0$  such that (4) is dissipative with respect to —

$$s(u(t), y(t)) = u^T(t) y(t) - \delta \|u(t)\|_2^2.$$

Finally (4) is strictly output passive if it is dissipative with respect to —

$$s(u(t), y(t)) = u^T(t) y(t) - \delta \|y(t)\|_2^2 \text{ where } \delta > 0$$

(1) The system (4) is finite gain  $L_2$ -stable with 11/21/2017  
 gain  $\leq \gamma$  if it is dissipative with respect BD/18-5  
 to —

$$s(u(t), y(t)) = \frac{1}{2} \gamma^2 \|u(t)\|_2^2 - \|y\|_2^2.$$

From dissipation inequality —

$$\int_0^t u^T(\tau) u(\tau) d\tau - \int_0^t y^T(\tau) y(\tau) d\tau \geq \Phi(x(t)) - \Phi(x(0)) \geq -\Phi(x(0))$$

This can be expressed as —

$$\int_0^t y^T(\tau) y(\tau) d\tau \leq \frac{\gamma^2}{2} \int_0^t u^T(\tau) u(\tau) d\tau + \Phi(x(0))$$

(2) Also, system (4) is finite gain  $L_2$ -stable if it  
 is strictly output-passive.

$$\int_0^t u^T(\tau) y(\tau) d\tau \geq \gamma \int_0^t y^T(\tau) y(\tau) d\tau + \beta \quad \gamma > 0, \beta \in \mathbb{R}$$

Therefore,

$$\begin{aligned} \int_0^t y^T(\tau) y(\tau) d\tau &\leq \frac{1}{\gamma} \int_0^t u^T(\tau) y(\tau) d\tau - \beta/\gamma \\ &\leq \frac{1}{\gamma} \int_0^t u^T(\tau) y(\tau) d\tau - \left(\frac{\beta}{\gamma}\right) + \frac{1}{2\gamma} \int_0^t \left(\frac{u^T(\tau)}{\sqrt{\gamma}} - \sqrt{\gamma} y(\tau)\right) \left(\frac{u(\tau)}{\sqrt{\gamma}} - \sqrt{\gamma} y(\tau)\right) d\tau \\ &= -\frac{\beta}{\gamma} + \frac{1}{2\gamma} \left(\frac{1}{\gamma} \int_0^t u^T(\tau) u(\tau) d\tau + \gamma \int_0^t y^T(\tau) y(\tau) d\tau\right) \end{aligned}$$

Hence,

$$\int_0^t y^T(\tau) y(\tau) d\tau \leq \frac{1}{\gamma^2} \int_0^t u^T(\tau) u(\tau) d\tau - \frac{2\beta}{\gamma}$$

Then, by restricting our focus to infinitesimal movements along trajectories of (4), we can express the dissipation inequality as —

$$\left(\frac{\partial \Phi}{\partial x}\right)^T f(x, u) \leq s(u, y) \quad (7)$$

This inequality is called the differential dissipation inequality.

Now assume  $\Phi: \mathbb{R}^n \rightarrow \mathbb{R}^+$  is a continuously differentiable (i.e.  $C^1$ ) storage function for the system defined by (4). Moreover,  $x^* \in \mathbb{R}^n$  is a strict local minima of  $\Phi$ , and the supply rate is such that

$$s(0, y) \leq 0 \text{ for all } y.$$

Then,  $x^*$  is a stable equilibrium of (4) when the external input is zero. To show this, define a Lyapunov function as —

$$V(x) = \Phi(x) - \Phi(x^*).$$

Clearly,  $V(x^*) = 0$  and  $V(x)$  is strictly positive for  $x$  in the neighborhood of  $x^*$ . Also,

$$\dot{V}(x) = \left(\frac{\partial \Phi}{\partial x}\right)^T f(x, 0) \leq s(0, y) \leq 0,$$

from the differential dissipation inequality.

### INPUT-TO-STATE STABILITY (ISS):-

Consider a function  $\beta: [0, \infty) \times [0, \infty) \rightarrow [0, \infty)$ . We call  $\beta$  to be a class  $K_\infty$ -function if  $\beta(\cdot, t)$  is a class  $K_\infty$  function for each  $t$  and  $\beta(x, t) \rightarrow 0$  as  $t \rightarrow \infty$ .

• The concept of input-to-stability state stability (ISS) provides a means to merge the concepts of internal (Lyapunov) stability and external (e.g. Operator approach based input-output stability) stability. ISS also formalizes the ~~the~~ concept of robustness with respect to disturbances. In what follows we consider the dynamics of the system to be governed by —

$$\dot{x} = f(x, u) \tag{8}$$

• This system (8) has the associated zero-system defined as —

$$\dot{x} = f(x, 0),$$

i.e. system with zero-input. Now, (8) is called O-GAS if the associated zero system is globally asymptotically stable.

However O-GAS does not necessarily mean that the system will yield a bounded output when excited by a bounded input. Consider —

$$\dot{x} = -x + (x^2 + 1)u.$$

Clearly the zero-system  $\dot{x} = -x$  is GAS. But there are some bounded inputs (which even converges to zero) which lead to diverging solutions for the state.

Consider,  $u(t) = \frac{1}{\sqrt{2t+2}}$

and,  $x(0) = \sqrt{2}$

Then,  $x(t) = \sqrt{2t+2} \rightarrow \infty$  as  $t \rightarrow \infty$ .

Moreover, if the input is identically 1, i.e.  $u \equiv 1$ , we have —

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$$\dot{x} = -x + x^2 + 1 = \left(x - \frac{1}{2}\right)^2 + \frac{3}{4} > 0$$

$$\text{and, } x(t) = \frac{\sqrt{3}}{2} \tan\left(\frac{\sqrt{3}}{2} t + \tan^{-1}\left(\frac{2x_0 - 1}{\sqrt{3}}\right)\right) + \frac{1}{2}$$

↑ this solution explodes in finite time.

Thus we need more conditions on the dynamics to ensure that the states will be bounded under bounded input.

• The system  $\dot{x} = f(x, u)$  (i.e. (8)) is input-to-state stable if there exist a class  $\mathcal{K}$ -function  $\beta$  and a class  $\mathcal{K}$ -function  $\gamma$  such that

$$\|x(t)\| \leq \beta(\|x(t_0)\|, t - t_0) + \gamma\left(\sup_{t_0 \leq \sigma \leq t} \|u(\sigma)\|\right)$$

for any initial condition  $x(t_0)$  and any bounded input  $u(t)$ .

Then, we can claim that for a system which is ISS, the following hold true —

i) The state will always be bounded for bounded inputs.

ii)  $x(t)$  is ultimately bounded by a class  $\mathcal{K}$  function of  $\sup_{t \geq t_0} \|u(t)\|$ , i.e. solutions will eventually be trapped inside a ball of finite radius.

iii) Whenever  $u(t) \rightarrow 0$  as  $t \rightarrow \infty$ , we have  $x(t) \rightarrow 0$  as  $t \rightarrow \infty$ .

iv) The origin of  $\dot{x} = f(x, 0)$  [the zero-system] is GAS.

- Let  $V(x)$  be a continuously differentiable function such that —

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$$\alpha_1(\|x\|) \leq V(x) \leq \alpha_2(\|x\|)$$

$$\text{and, } \left(\frac{\partial V}{\partial x}\right)^T f(x, u) \leq -W(x) \quad \forall \|x\| \geq \rho(\|u\|) > 0$$

where  $\alpha_1, \alpha_2 \in K_\infty$ ,  $\rho \in \mathcal{K}$  and  $W$  is a continuous positive definite function. Then, the system  $\dot{x} = f(x, u)$  is ISS with  $\rho = \alpha_1^{-1} \circ \alpha_2 \circ \rho$ .

- $\dot{x} = -x - 2x^3 + (x^2 + 1)u$

Let,

$$V(x) = \frac{1}{2} x^2$$

$$\begin{aligned} \dot{V}(x) &= \left(\frac{\partial V}{\partial x}\right) f(x, u) \\ &= -x^2 - 2x^4 + (x^2 + 1)xu \\ &= -x^4 - x^2(x^2 + 1) + xu(x^2 + 1) \\ &= -x^4 - (x^2 + 1)(x(x - u)) \\ &\leq -x^4 \quad \text{when } |x| \geq |u| \end{aligned}$$

Therefore this system is ISS with —  
 $\rho(\sigma) = \sigma$